

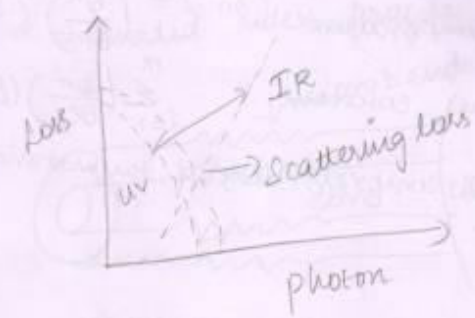
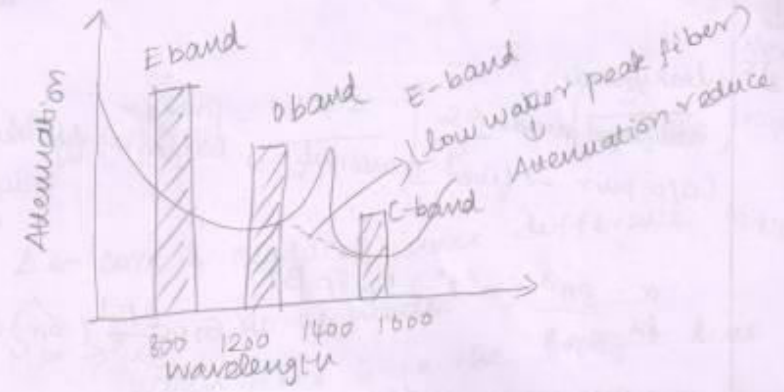
$P(0)$ → Initial power
 $P(z)$ → distance
 Attenuation → dB/Km
 Power reduce
 initial → signal high
 distance ↑ → many loss introduce
 (Scattering, absorption) impure → pure
 Absorption → atomic defect / material

$$\alpha \text{ (dB/km)} = \frac{10}{z} \log \left[\frac{P(0)}{P(z)} \right] =$$

Atomic defects: missing of O_2 ion
 missing of molecules / cluster
 main reason Ionisation radiation: (UV rays)
 In space Ionisation rad → light
 medical app. x-rays
 Indust app. nuclear reactions
 Reduce atomic defects
 fiber → pure silica core → radiation light
 2) Impurity → cleaning process → water
 dissolve in fibre

Pure silica
 3) Particular wavelength \rightarrow act as a bad conductivity \rightarrow absorb
 (UV, IR wavelength)
 \downarrow other waves propagate
 $d_{uv} = c e^{E/E_0}$
 Wavelength is important for attenuation

IR: $d_{IR} = 7.81 \times 10^{-11} \exp\left(\frac{-4840}{T}\right)$



fiber is inserted into cable \rightarrow loss due to misalignment \rightarrow micro bending
 Radiation loss \rightarrow cable bend \rightarrow radius \downarrow \rightarrow macro bending (due to fibre loss)

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glass small

Scattering loss:
 due to
 { microscopic variation in the material density
 compositional fluctuations
 Structural inhomogeneous
 Structural Defects arising during fabric

Types:
 Linear, Non-linear → opt power → diff freq → diff dir

Rayleigh
 ↓
 UV region
 ↓
 in all direction
 (λ⁻⁴)

leaky mode,
 radiated mode
 (o/p power → fiber transmit → linear → one mode
 transfer
 differ mode)

$$\alpha = \frac{8\pi^3}{3\lambda^4} (n^2 - 1)^2 K_B T F \beta T$$

$$\alpha = \frac{8\pi^3}{3\lambda^4} (\delta n)^2 \sigma$$

n → Refractive index
 TF → fictive Temperature $(\delta n^2)^2 = \left(\frac{\partial n^2}{\partial P}\right)^2 (\delta P)^2$
 KB → Boltzmann's constant $\sum_{i=1}^m \left(\frac{\partial n^2}{\partial C_i}\right) (\delta C_i)$
 βT → Isothermal compressibility of the material

Bending loss:
 occur due to manufacture of fibre
 Bending radius of curvature → occur loss

Large radius loss
 or
 Simply bending loss

1. Macro Bending (radius of curvature > fibre diameter)
2. Micro Bending (radius of curvature ↓, loss)

Reduce macro bending
 by index diff large
 bend
 misalignment
 fibre axis →
 Small fluctuation

mode coupling loss

cladding
core
field distribution
curved fiber

field distribution same \rightarrow total \downarrow field distribution distorts
Higher modes \leftarrow less \downarrow information $>$ Speed of the light

Normal transfer mode propagation

$$M_{eff} = M \left\{ 1 - \frac{\alpha + 2}{2\alpha\Delta} \left[\frac{2a}{R} + \left(\frac{3}{2n_2 k R} \right)^{2/3} \right] \right\}$$

$\Delta \leftarrow$ core & cladding index difference

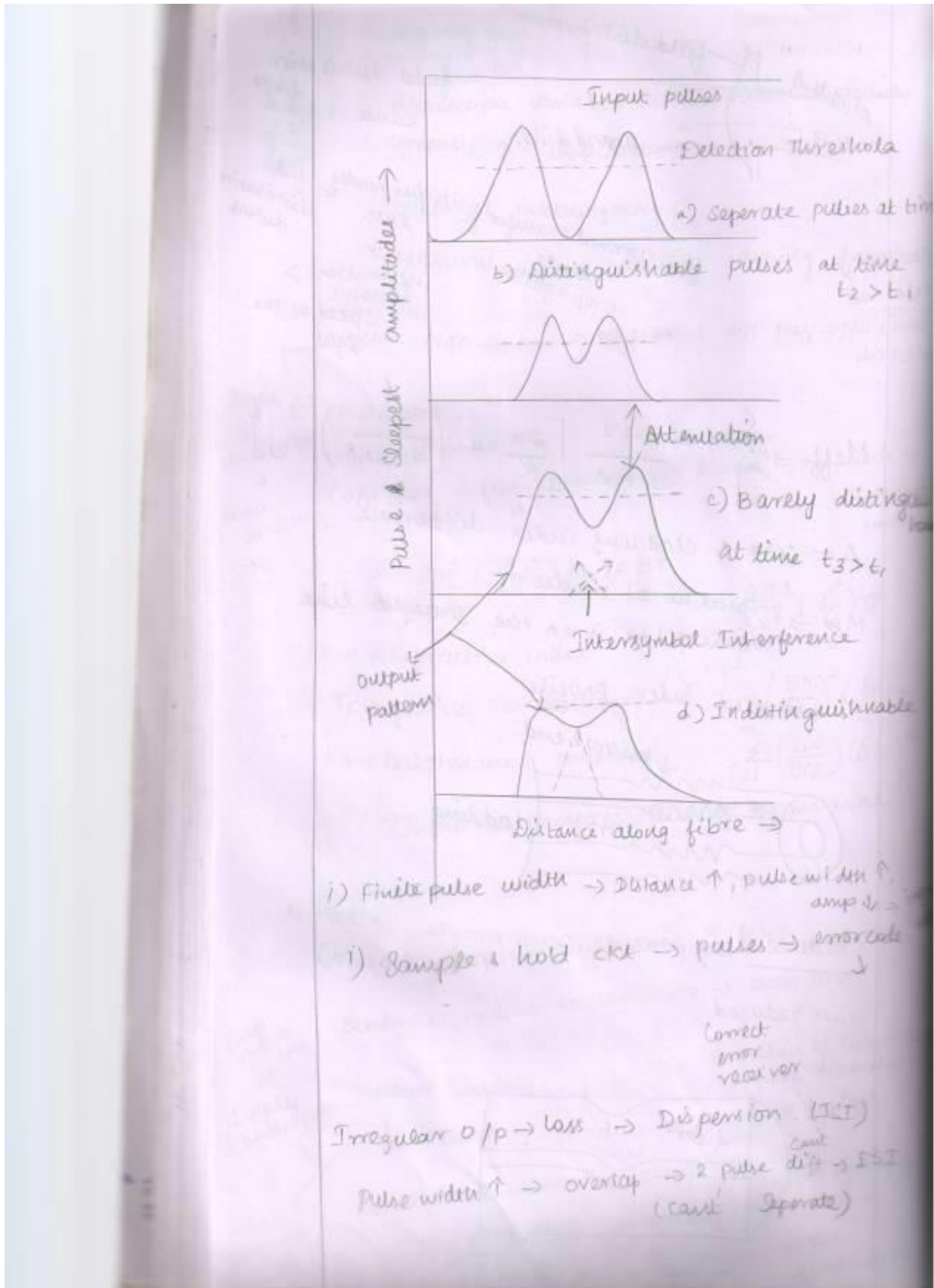
$M_{st} \rightarrow$ Total no. of modes when fibre is in the straight line

$\alpha \rightarrow$ Graded index profile

\downarrow microbend
core
cladding

Reduce: By placing compressible Jacket it can reduced. (20-500 G.Pa)

fiber
jacket



1. Inter modal (modal delay) → multimode fibre

2. Intra modal
 (Group Velocity dispersion or chromatic dispersion)

↓

Single mode fibre
 (due to narrow spectral width)

↓

Band of frequency
 (Range of wavelength)

Pulse broadening vary

Types:

- * Material dispersion
- * Waveguide dispersion

3. Polarized dispersion (alignment & disturb)

↓

Orthogonal polarization

Modal delay: Multimode fiber

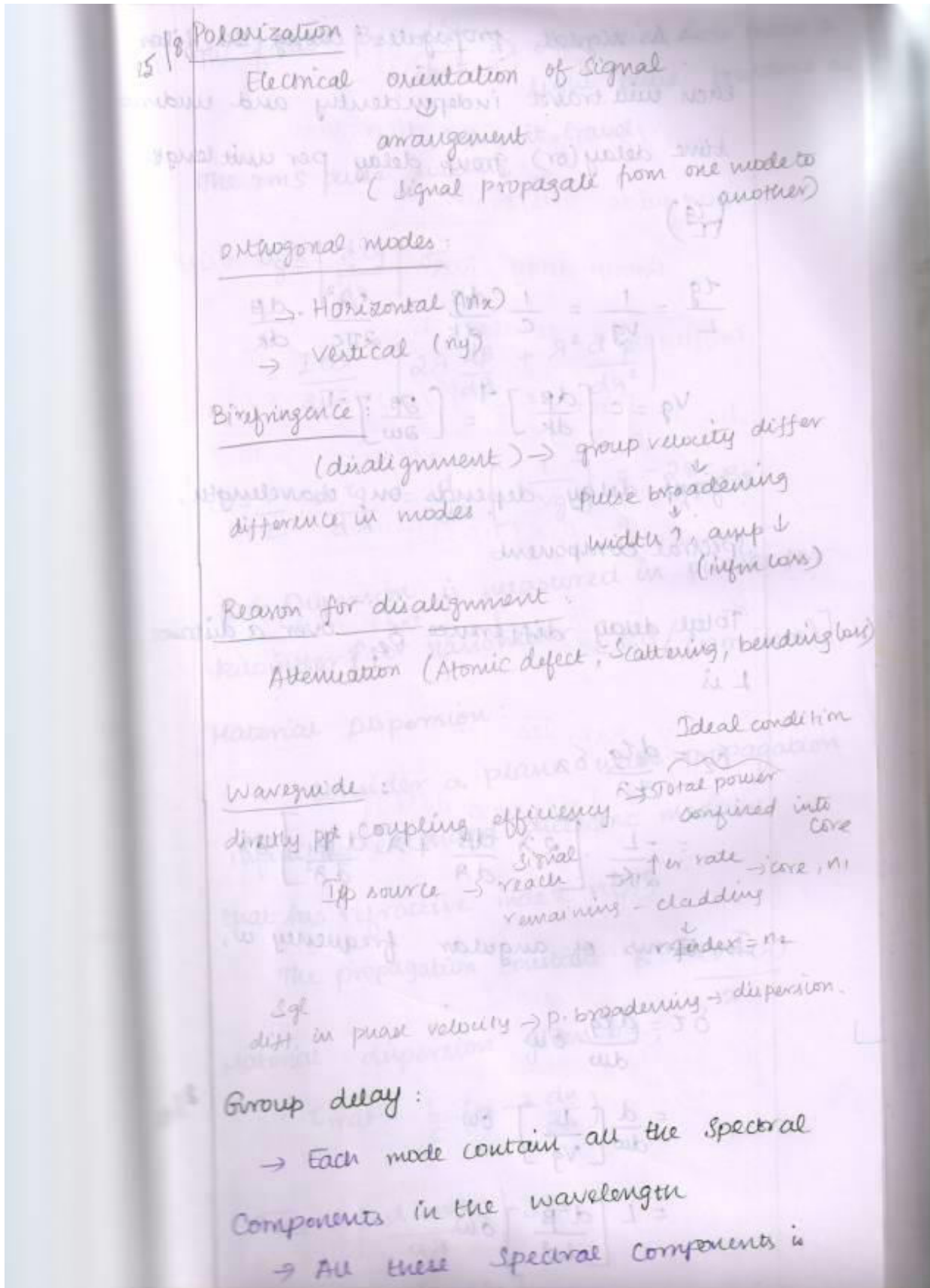
$$\Delta T = T_{max} - T_{min} = \frac{n_1}{c} \left[\frac{L}{\sin \phi_c} - L \right]$$

$$= \frac{Ln_1^2}{cn_2} \Delta$$

$$\Delta T = \frac{Ln_1 \Delta}{c}$$

T_{max} = Time taken by fundamental mode
 Time taken by higher order mode

Additional notes from image:
 - Pulse broadening → wavelength (single propagate w)
 - Group Velocity → Velocity Equal
 - (diff in time) (Vg) vary
 - Pulse broadening
 - R.I.P. Speed
 - Axis → Fundamental mode
 - Graded index fiber (refractive index) (short time period)
 - Higher order mode (long time period)



→ As signal propagates along the fibre each will travel independently and under time delay (or) group delay per unit length

$$\left(\frac{\tau_g}{L}\right)$$

$$\frac{\tau_g}{L} = \frac{1}{v_g} = \frac{1}{c} \frac{d\beta}{dk} = -\frac{\lambda^2}{2\pi c} \cdot \frac{d\beta}{d\lambda}$$

$$v_g = c \left[\frac{d\beta}{dk} \right]^{-1} = \left[\frac{\partial \beta}{\partial \omega} \right]^{-1}$$

group delay depends on wavelength,
Spectral component

Total delay difference δ_2 , over a distance L is

$$\delta_2 = \frac{d\tau_g}{d\lambda} \delta\lambda$$

$$= \frac{-L}{2\pi c} \left[2\lambda \frac{d\beta}{d\lambda} + \lambda^2 \frac{d^2\beta}{d\lambda^2} \right] \delta\lambda$$

In terms of angular frequency ω ,

$$\delta\tau = \frac{d\tau_g}{d\omega} \delta\omega$$

$$= \frac{d}{d\omega} \left[\frac{L}{v_g} \right] \delta\omega$$

$$= L \left[\frac{d^2\beta}{d\omega^2} \right] \delta\omega$$

The factor $\beta_2 = \frac{d^2\beta}{d\omega^2} \Rightarrow$ determine how much a light pulse broadens as it travel.

The rms pulse width,

$$\sigma_g = \left| \frac{d\tau_g}{d\lambda} \right| \sigma_\lambda$$

$$= \frac{L\sigma_\lambda}{2\pi c} \left[2\lambda \frac{d\beta}{d\lambda} + \lambda^2 \frac{d^2\beta}{d\lambda^2} \right]$$

$$D = \frac{1}{L} \frac{d\tau_g}{d\lambda} = \frac{d}{d\lambda} \left[\frac{1}{v_g} \right] = -\frac{2\pi c}{\lambda^2} \beta_2$$

$D \leftarrow$ Dispersion is measured in picosec per kilometer $\frac{1}{3}$ per nanometer $[P.S / (nm \cdot km)]$

Material Dispersion:

consider a plane wave propagation infinitely extended dielectric medium

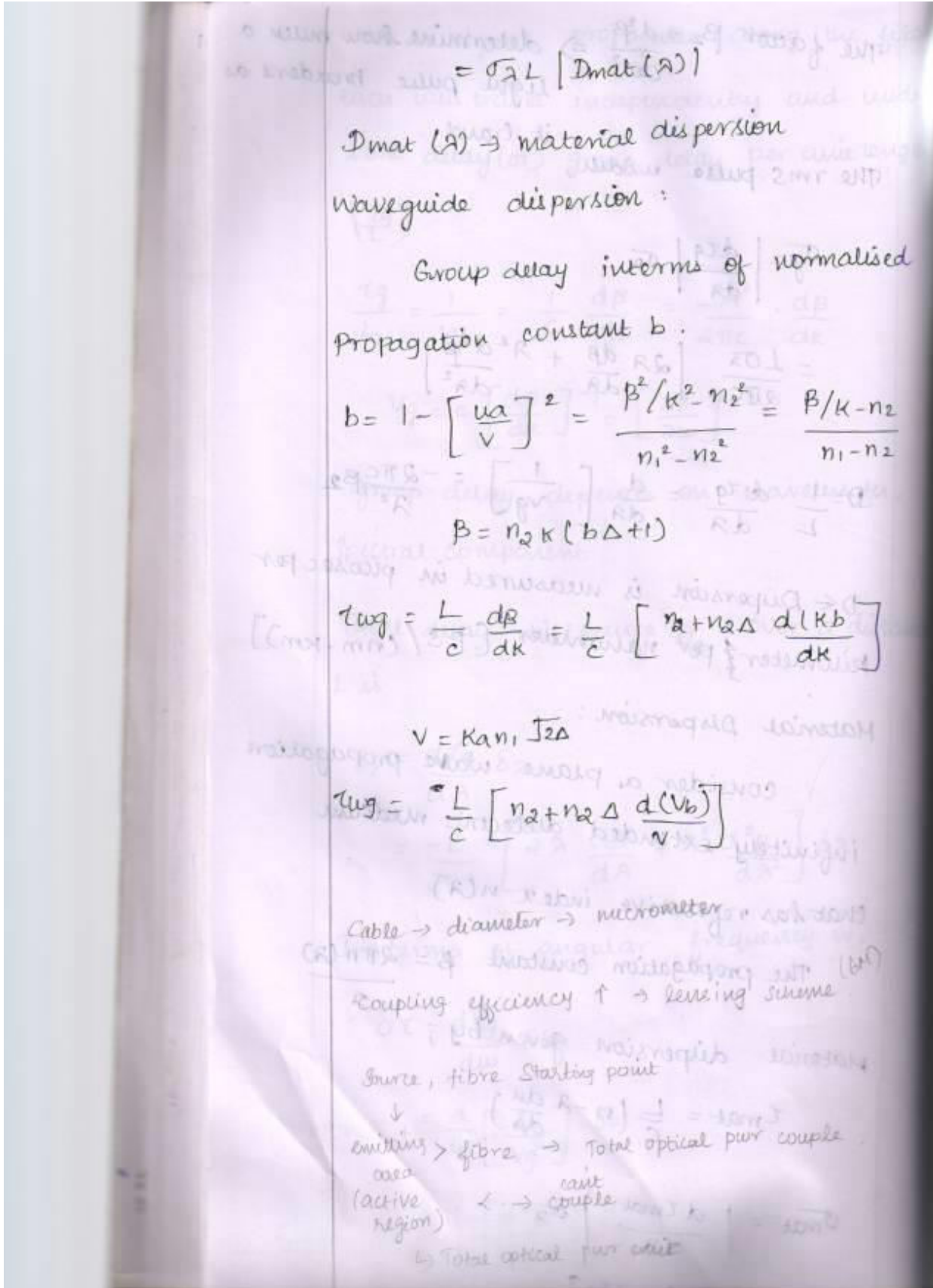
that has refractive index $n(\lambda)$

$$\text{The propagation constant } \beta = \frac{2\pi n(\lambda)}{\lambda}$$

Material dispersion given by,

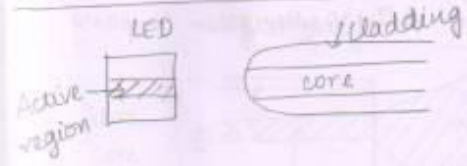
$$\tau_{mat} = \frac{L}{c} \left(n - \lambda \frac{dn}{d\lambda} \right)$$

$$\sigma_{mat} = \left| \frac{d\tau_{mat}}{d\lambda} \right| \sigma_\lambda$$

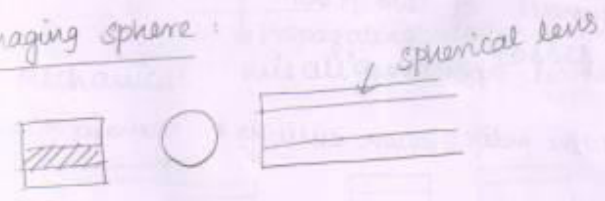


LENS kept blur
 LED & fibre → active region → Total optical ^{part} coupled to fibre
 (fibre small) ↑ coupling efficiency

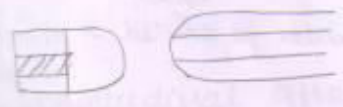
Rounded End Fiber



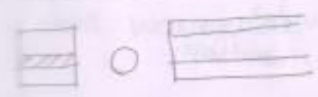
Imaging sphere :



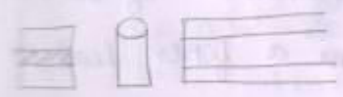
Spherical surfaced LED and Spherical Ended fiber :



Non-Imaging Microsphere :



Cylindrical lens



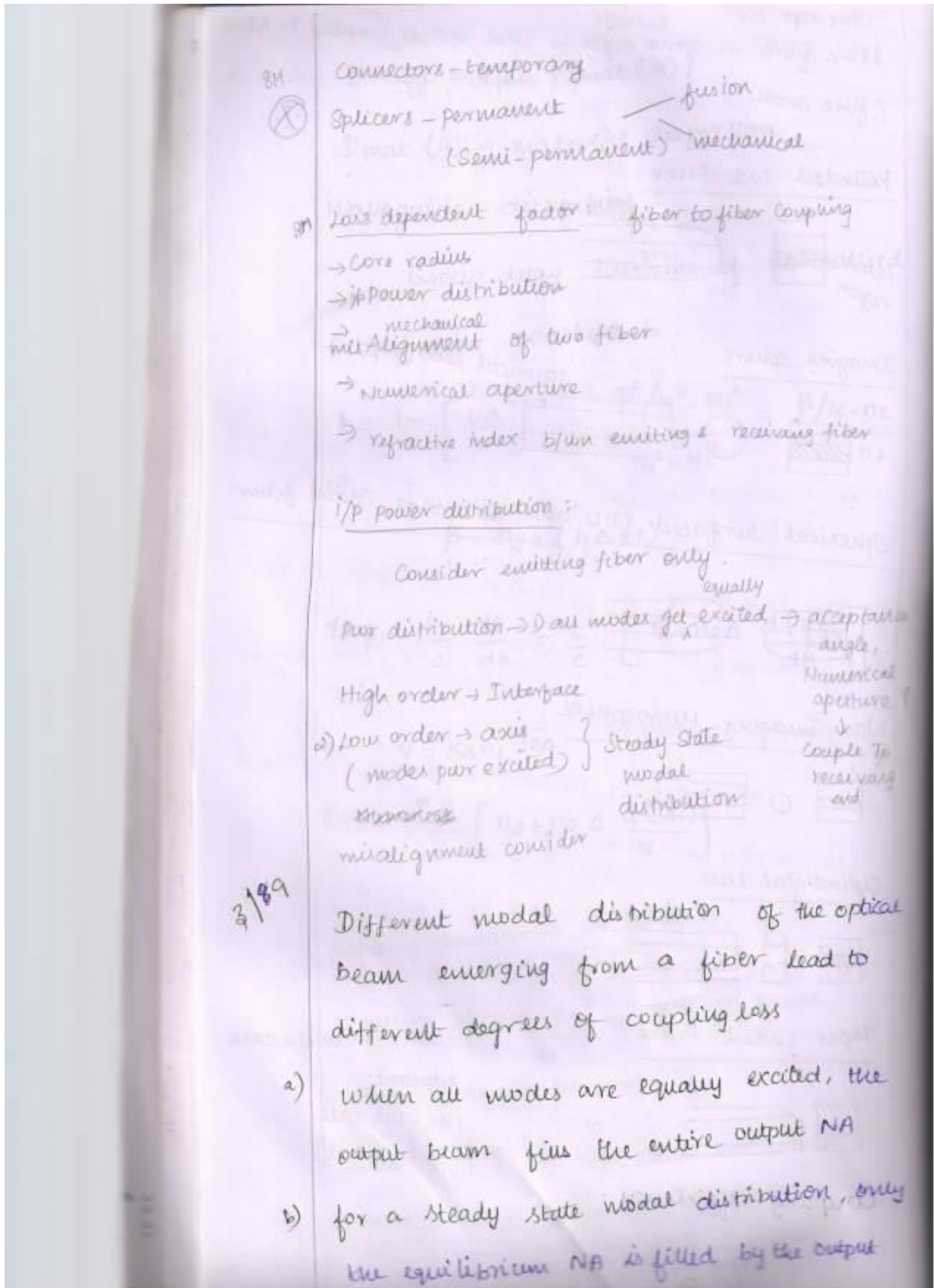
Taper Ended Fibre :



some manufacture attached
 1m - pit tail
 cable (flylead)

Coupling efficiency :

$$\eta = \frac{P_2}{P_3}$$



cladding
fibre core
all modes equally excited
full numerical aperture of fibre
fully filled fibre core

fibre core
Equilibrium
Propagating modes in the steady state
fully filled fibre core

Mechanical misalignment losses:

a) lateral
b) Longitudinal (end separation)
c) Angular

Longitudinal offset effect
Losses due to differences in the geometry and waveguide characteristics of the fibers

$$L_F(a) = -10 \log \frac{(aR)^2}{(aE)^2} \text{ for } aR \leq aE$$

$$L_F(a) = -10 \log \frac{(NAR)^2}{(NAE)^2} \text{ for } NAR \leq NAE$$

E & R Subscripts refer to emitting & receiving fibers

End preparation technique

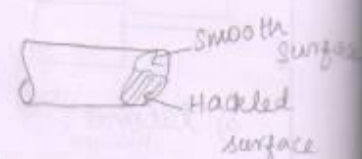
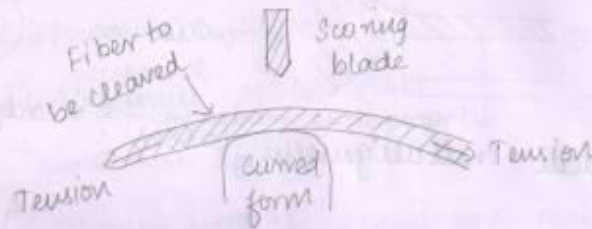
- 1) Sawing
- 2) Grinding

4) Controlled fracture

5) Laser cleaving

Fiber end face:

curved position \rightarrow Pressure



Fiber end defects

Fiber to Fiber Joint

Fiber to Fiber Coupling loss

$$L_f \text{ [dB]} = -10 \log \eta_f$$

Low loss fiber-fiber joints are either:

1. splice (Permanent bond)
2. connector (demountable connection)

Common end face defects:

- Hip
- Roll off
- chip
- Hackle
- Mist
- Spiral or Step

Splicing

Process of permanent connection of two pieces of optical fibers.

Fusion Splicing

Electric melt → mould
arc
(heat)

Splice → joint made by overlapping two ends & joining them

Splicer → Mechanical device for joining two pieces of

V-groove optical fiber splicing

V-shape → adhesive gum

Paper or film or magnetic tape

Elastic Splicing

Two sides → elastic material
core radius < insertion hole
expand → no misalignment

Types:

1. Fusion Splice
2. V-groove optical fiber tube splicing
3. Elastic Splicing