UNIT-V. (IS 1905-1987 BRICK MASONRY! Beick marony is a unfiel mass abtained Systematic arrangement of laying bricks and bonding to gither with martax charification of well: (page No: 4) in Cavity wall. I.3 12) faced wall. 3. Venewed wall. A. Partition well. 5, panuled wall. 6. Sheat wall to load bearing wall. datural Suprait of Itabithy > (page No: 5) (i) to limit the stendamen ratio of a majority element so as to give to reduce paribility of butting of the menter due to vertical loads. s. to ordict haricantal component of do four so as to enum stability of structure against over turning

17)	
	STABILITY: (page No: 6)
	is simple states reaction at the paint
ablained	of lateral Supposet to all the lateral load and
Sagara .	The second second
icke	25% of total vertical load that wall
100	based estumn in designed to easily at
	point of lateral Support
	Lolumn maioney:
	An inolated vertical load bearing
	member, with the of which does not
	exceed of time of thickness.
	Pier ! " tok were t training many
2	a tuck section farming integral
	facility a wall placed at interally along
_	the wall to write stiffners wall law
5)	to early vertical concentrated load.
8 .	Buthun:
4	sa pier of maronry built as an
hi	integral and of
ь	integral part of wall and projeting
,	from erg either are both durfacel.
罗	Stendences ratio:
q	
	It is the natio of effective length
	(ac) effective height to effective thickness of
	The state of the s

	10
Duign loads: - > (page No:15)	Lyingth
Load to be taken in to consideration	Came
far during moreoney component of a	Step 2
Structure of dead board ,	Co
(i) dead load of week, dead load	1
flower f dead touch of woof.	>
in live load of flowers theofered	
in, wind load on wall & cloping	c/
de la	Shpi
(iv) decemie face.	Page
effective height: (page No: 11)	
—	fua
determine the allowable axial lead on the color	and and
of Sire 30 cm × 60 conclucted in fact class	Lan
built work in 1:6 cement marter wing	
modular briet die of 200 x 100 x 200, height	-1
of nier b/w the footing and lough Mas 5.1 m	Step
strength of will may be taken as 10 Mpa	
gen:	
solamn Sou = 300 x 600 mm.	P
height of piece = 5-1 m.	

strength of writ = 10 N/mm2 Cement mortan = 1.6: step 2! effective height of colourn. 15 1905: 1987 => effective height = 1.00 H. Step 2: Baile compression stress: - (fc). Page No: 16. Fu H, H2 NIH2 H3. L1 12 -> Table 1 from table of the guide of narrar was confarined as M2 for severed martax xálio 1:6 from table No: 8 the baric compression streets = Bain comprision stress = 0.81 2/mm2 Step 3: drea of Reduction factory: Aura of edumn = 300 x too = 180000 mm2 = 0.18m2. Page No:16 The wall distingt and of the column

the calculation of compression street. Ka = 0.7+ 1.5A, A 1	step
= 0. ≠ + 1.5 (4g)	
Step 4: Shape modelantin 1	
Step 4: Shape modification factor for marony unit:	Step
hight to weath water >	
200/ => 1.	
- facus table 10 Shape modification factoris = 1.1.	axi
Stas: 1 7	
Step 5: load factor.	
a for axial load > 1 . for eccentrical > 1.2 . $K_{L} = 1 \rightarrow C$ for anially loaded	

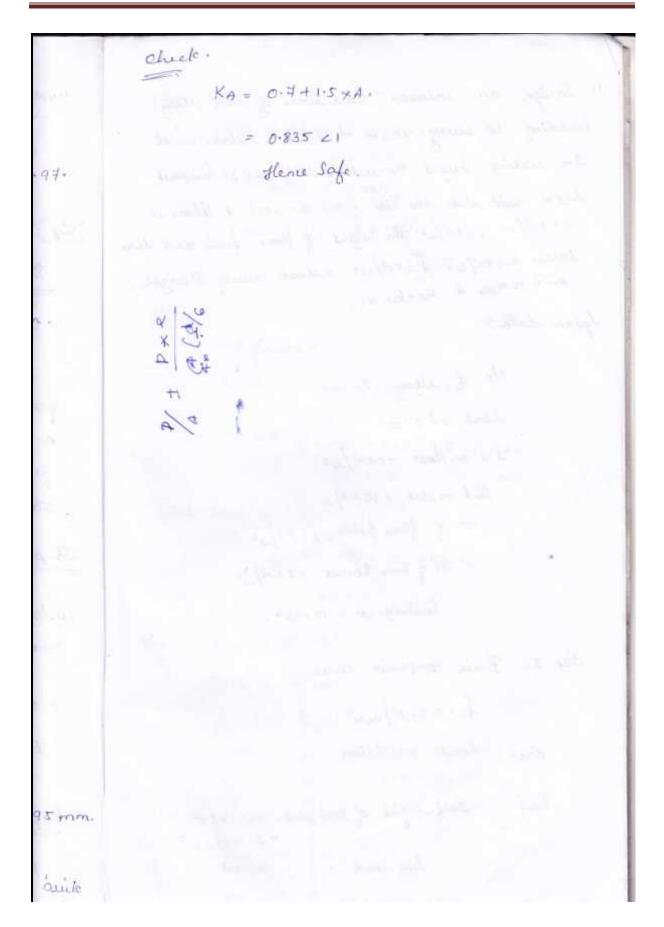
2, of column of Sine 300 x \$50 mm, concluded in	3
1st class buick in 1:6 Cement martax ming	
modular brick Sire of 200 ×100×200 height of	
Ner b/w feeling and top slab is 4.5 m., the	
Shength of write may be taken at 10 M/mm	
Calculate compression Muss load for	
applied at eventuaty of 100 mm.	4
(i) Sine = 300 + 560	
height = 1.5	
Sing buill = 200+100+200.	
Shingt = 10 N/mm2	oL.
Coment marton = 1:6.	24
10	
= effective height	ی
=> effective height: 1× 4.5	
= Δ.5 m.	
(ii) Bain compression etres.	a l
	Sty
€ 0.81 N/mone2.	

eled in	3 does of reduction factor:
aing	=) A = 300 x 550 = 165000 mm
ght of	= . 165 mm 2
., the) Ka = 0.7 + 1.5 A.
1/nem2	> 0.7+1.5 (0.165)
à.	= 0.94
	4 shape modification factor.
	200/ -> 1
	> 20% => 1
	=) Kp=1.1
	Step 5! lond factor!
4	KL = 1.25, (for eccentrical column).
	Step6: stender ne => . 4-5/ = 15. 600 = 0.16.
	strus auduction factor => 0.66.
	÷>
	Step 7 Compression Strees:
	fca = fcx kAxkpxkl x KSF

I duign a buick column of height 3 m to wed Carry an axial load of 100 KM winth of prior is limited to 1/2 of Harnal brick for architectural reakeon, adopt cement line marker of regrantion 1:1:6 & ful clas buick, with 10 upa Strength. the column may be taken as tended sectuaine. given: anial Load :- 110 KN. height = 3 m : min viatio: 1:1:6 Strength of writ : 10 mpa. end condition : fixed restrained class of brick . 1st class. unle Step 2 : eff height page No: 11. Table - 4 Condition -2 > of het > 3 x 0.85 Step2: stendures viatio:

undth of normal buck = 228 mm. > off ht/ 2.550/ Stips compression etters. Page No: 16. > Baric compresion Stress > 0.96 1/mh2 =) fc = 0.96 Mmm 2 from table I the grade of marter was conferred as 6.1120 for coment mater ratio 1:1:6, from table - 8 ; the baile compression Street = 0.96 N/mm 2 Step 1 Lua of auduction factor. unless the length of pier -d = it known, the area & A cannot be found. In hence > KA is unknown. Normally KA is varied blu ofto 1, let us take the average value of 0.875 Step 5 : Shape seduction factor : Page No: 17 table: 10

Step 6: Streets actuation faction => Ks = 0.97 100+0.95/2.0.97. Step 1) load factor) FL = 1 faraial loaded. column. Step 8: Compress stees: fear = fe + KA + Kpx KSF + FL = 0.96 × 0.8 75 ×1×0.93×1. Stree = P/A 0-814 = 110×10³/ /342×d.) d= 395.13 mm. the sixe of the column is 228×395 mm. Here the column Lection of 1x/2 x 2 with



" Derign as interior cross ware of two stary Hoos building to early soon third R-cc. Mab. with 3m healing hught the wall is stiff and it dunnant 2.65 m wide clab . the live load on soof of Aloon is 1.5 KN/m2 42KN/m2 the height of floor fruit and line luan 0.2 KN/m2 & 2 KN/m2. adopt cring Stungth. unit 10 Mps + Mostles M. Given data : No. of story = 2. Slab +k: 100 1.1 on floar = LKN/m2 lied on Mab = 15 KN/M. wt of floor finish = 02 KN/mc wo of line tower = 2 KH/m2 lunhing it = 10 mpa. Step 1: Baile comprision steers. fc = 0.96 N/mm2. Step 2: load calculation Roof Self weight of Roof Mab = 1x0.1x25 live load : 1.5 11

```
floor elab:
      S.w. of Slab = 1x0.1 x25
   live load = 2 km/ne
          wt. of # = 0.2 Follow.
       wed wood x.
        adopt Thickness of wat = 100 mm.
            wt of wall - 1×0.1×3×2×20 -
=12. (20-runib waghty)
Anuk)
 Total load on wall
           => [ (6+4.7) 2.65] + 12.12
              = 40.35 KN/m.
step 3: effective height.
        Bothe end fixed.
         => effect height = 0.75 H
                        : 2250 mm.
 Step 4. Mendernes ratio:
       eff hught = 2250/
```

From table of the maximum blendernes natio for two Starry building should not be greater than 27. Steps . Stees reduction faction. Ef = 0.53 N/mm2 Page No:16 Stept :- Permueble Compresion stees: fac = ks x fc. = 0.5\$ × 0.96 = 0.508 N/mm2. actual Compune etus = P/A. Aua: (Thickno: Ineter (1000×100)

> 6=0.403 kd/m2 N/mn2. > 0.4 20.508. Henre Safe.

2 Duign extures wall of a building to early 100 mm thick Rc Mab. 3 m reling height support contins is fixed, writinged, live load on wood is 2 EN/m2 , about crushing ities the of built unit as 10 N/mn2 , M1 - mouton, -. given data: height : 3 m. live load on acof = 2 4 N/m. Slungth = 10 N/mm2. 100mm their Re Mab. Bain Conjunios elius: ≥ 0.96 N/ww1. load calcutation :-Sey weight > 1 x 0.1 x 25 = 2.5 EN/w. live load = 1 EN/m. flow. Schwanger = 2.5

```
wall.
    t = 230 mm. (extrior avail).
      => 1x0.1 x 3x2 x 20
          => 12.
   Total load.
        => (A.5+ a.+)3)+ (12).
        = 39 KN/m.
 step 3 eff high
        > kat + 0.85 H
               > 2.550 m.
  Stendunus vicdis
          D 2550/ = 11.08 427.
        . Hence stefe.
5. utu vidudios factas
        Ks = 0.86
 6, permuble comprove etrus
           =) fac = 0.86x 0.96
```



	step 6: shus acoluction factor:
4.	Page No: 16 table No: 9.
	Stendoner activ = effective height
	least latual dimension
	> 5.1/ _{0.3} = 17.
oney	-> decrease -73 + 0.67
0	=> stress reduction .73 + 0.67 Step 7: Jaclan = 0.7.
	Step 7: Compression street:
	fea = fe x KAX Kp x Kl x KSF
- 1	= 0.81 × 0.97 × 1.1 × 1 × 0.7
	= 0=604 N/mm2
1.7 6	axial land. fea = 1/A.
	· Limite on the
	=> P = fca x A.
nelle.	= 0.604 × (0-18) 300+600).
	= 108.727103
	= 108.72 KN.
	= 108-12 = 1
1 60	